

If we assume  $v_n$  to be zero and  $v_s$  is negligibly small before entering the plug, (2) may be integrated along its length to obtain the steady-state solution

$$\frac{1}{2} \frac{\rho_s v_s^2}{\rho} = S\Delta T - \frac{\Delta P}{\rho} \quad (3)$$

using the fact that  $\rho_n + \rho_s = \rho$  and  $\partial v_s / \partial t = 0$ .

The rate of heat withdrawal from the plug is  $Q \simeq L\dot{m}$ . (The exact expression includes the term  $TS\dot{m}$ , but this is small compared to  $L\dot{m}$ .) If the cross-sectional area of the solid portion of the plug,  $A'$ , is several orders of magnitude larger than the channel cross-sectional area,  $A$  (see description of plug below), we may assume that the heat flow is dominated by the thermal conductance of the metal, namely,  $kA'/l$ . Under these conditions,  $\dot{Q} = C\Delta T$  and hence,

$$\Delta T = \frac{L\dot{m}}{C} \quad (4)$$

Also,  $v_s$  may be expressed in terms of  $\dot{m}$  as

$$\rho_s v_s A = \dot{m} \quad (5)$$

Substituting (4) and (5) into (3) gives the relation

$$\frac{\dot{m}^2}{2A^2\rho_s} = \frac{\rho SL\dot{m}}{C} - \Delta P \quad (6)$$

This is a quadratic equation for  $\dot{m}$  in terms of known parameters whose solution is

$$\dot{m} = \frac{\rho SL/C \pm \sqrt{(\rho SL)^2/C^2 - 2\Delta P/A^2\rho_s}}{1/A^2\rho_s} \quad (7)$$

Insertion of known values for  $S$ ,  $L$ ,  $C$ ,  $P$ , and  $A$ , for an aluminum plug of the dimensions described below and in the range of 1.6 to 2°K shows that the second term under the radical is much smaller than the first. Expanding to a first order provides us with the following two expressions:

$$\dot{m} \simeq \frac{\Delta PC}{\rho SL} \quad (8a)$$

and

$$\dot{m} \simeq \frac{2\rho_s\rho SLA^2}{C} - \frac{\Delta PC}{\rho SL} \quad (8b)$$

Assuming that the pressure drop in the pumping line is negligible,  $\Delta P$  is simply the vapor pressure inside the dewar. Since (8b) yields flow rates greatly exceeding  $v_{crit}$  in almost any physically realizable situation, it is rejected as violating the assumptions on which the derivation is based.

By substituting approximate temperature dependences of  $C$ ,  $S$ , and  $\Delta P$  into (8a), we obtain the temperature dependence of  $\dot{m}$  as

$$\dot{m} \propto e^{-8.9/T} T^{-3.6} \quad (9)$$

This expression is monotonically increasing in the temperature range from 0°K to